Lloyd's Register

Rules and Regulations for the Classification of Special Service Craft, July 2012

Notice No. 4

Effective Date of Latest Amendments:

See page 1

Issue date: February 2013

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RULES AND REGULATIONS FOR THE CLASSIFICATION OF SPECIAL SERVICE CRAFT, *July 2012*

Notice No. 4

This Notice contains amendments within the following Sections of the *Rules and Regulations for the Classification of Special Service Craft, July 2012*. The amendments are effective on the dates shown:

Part	***Chapter***	***Section***	***Effective date***
1	2	2	1 July 2013
3	1	3,7	1 July 2013
3	3	2	1 July 2013
3	4	7	1 July 2013
5	1	2	1 July 2013
6	2	4	1 July 2013
7	2	4	1 July 2013
8	3	1	1 July 2013
8	7	2	1 July 2013

It will be noted that the amendments also include corrigenda, which are effective from the date of this Notice.

The *Rules and Regulations for the Classification of Special Service Craft, July 2012* are to be read in conjunction with this Notice No. 4. The status of the Rules is now:

Rules for Special Service Craft	Effective date:	July 2012
Notice No. 1	Effective date:	1 October 2012
Notice No. 2	Effective date:	1 January 2013 & Corrigenda
Notice No. 3	Effective date:	1 January 2013 & Corrigenda
Notice No. 4	Effective date:	1 July 2013

Part 1, Chapter 2
Classification Regulations

Effective date 1 July 2013

■ *Section 2*
Scope of the Rules

2.1 Applicable craft types

2.1.2 The following craft types will be considered upon request on the basis of the Rules:

(a) Amphibious air cushion vehicles.
(b) Rigid inflatable boats.
(c) Hydrofoil craft.
(d) Foil assisted craft.
~~(e) Craft as defined 2.1.1(a) to (e) constructed from wood or wood/composite combinations.~~
~~(f) Other craft constructed from composite materials.~~
~~(g)~~(e) Craft with a Rule length, L_R, less than 24 m and draught to depth ratio greater than 0,55.

Part 3, Chapter 1
General Regulations

Effective date 1 July 2013

■ *Section 3*
Equivalents

3.1 Alternative arrangements and scantlings

(*Part only shown*)

3.1.2 Where calculation procedures other than those available ~~within the LR *Software Guide*~~ from software published by LR are employed, supporting documentation is to be submitted for appraisal and this is to include details of the following:

■ *Section 7*
Inspection, workmanship and testing procedures

7.3 Testing procedures

Table 1.7.1 Testing requirements (*Part only shown*)

Item to be tested	Testing procedure	Testing requirement
Double plate rudders	~~Structural (1), (5)~~ Leak, *see* Note 5	~~2,4 m head of water, and rudder should normally be tested while laid on its side~~ *See* 7.3.4

Part 3, Chapter 3
Control Systems

Effective date 1 July 2013

■ *Section 2*
Rudders

2.19 Pintles

Table 3.2.11 Pintle requirements (*Part only shown*)

Item	Requirement
(1) Pintle diameter (~~measured outside liner if fitted~~), *see* Note 2	
NOTES 1. Proposals for higher pressures or other materials will be specially considered on the basis of satisfactory test results. 2. The length of the pintle housing in the gudgeon is not to be less than the maximum pintle diameter.	

Table 3.2.12 Rudder couplings to stock (*Part only shown*)

Arrangement	Parameter	Requirement
(2) Conical couplings	$\overline{p}$	$\dfrac{P_R \theta_t \overline{\delta}_{ST} + 4M_T \sqrt{K_2\left(\left(\dfrac{P_R \overline{\delta}_{ST}}{2M_T}\right)^2 + 1\right) - \left(\dfrac{\theta_t}{2}\right)^2}}{\text{~~5,66~~ } 5{,}03\ \overline{\delta}_{ST}^2\, l_t \left(K_2 - \left(\dfrac{\theta_t}{2}\right)^2\right)}$
	P_u	Approximately equal to ~~2,83~~ $0{,}8\,\pi\,\overline{p}\, l_t\, \overline{\delta}_{ST} \left(K_3 + \dfrac{\theta_t}{2}\right)$

2.21 Conical couplings

2.21.1 Where a rudder stock is connected to a rudder by a keyless fitting, the rudder is to be a good fit on the rudder stock cone. During the fit-up, and before the push-up load is applied, an area of contact of at least ~~90~~ 80 per cent of the theoretical area of contact is to be achieved, and this is to be evenly distributed. The relationship of the rudder to stock at which this occurs is to be marked, and the push-up then measured from that point. The upper edge of the upper mainpiece bore is to have a slight radius. After the final fitting of the stock to the rudder, positive means are to be used for locking the securing nut to the stock.

Part 3, Chapter 4
Closing Arrangements and Outfit

Effective date 1 July 2013

■ *Section 7*
Portlights, windows and viewing ports, skylights and glass walls

7.12 Deadlights and storm covers

(*Part only shown*)

7.12.6 For craft in **Service Groups G4** and **G5**, storm covers or deadlights are required as follows:

(f) Windows in the shell ~~above Position 2~~, located at least one standard height of superstructure above the lowest Position 2 deck, are to be provided with strong portable internal storm covers for 25 per cent of each ~~window~~ size, with means of securing being provided at each window.

Part 5, Chapter 1
General

Effective date 1 July 2013

■ *Section 2*
Direct calculations

~~**2.2 Special Service Craft Software**~~

~~*2.2.1* LR's direct calculation procedures and facilities are summarised in a publication entitled the LR *Software Guide*.~~

~~2.3~~ 2.2 Submission of direct calculations

(*Part only shown*)

~~*2.3.1*~~ *2.2.1* In cases where direct calculations have been carried out ~~using procedures available in the LR *Software Guide*~~, the following supporting information is to be submitted as applicable:

Existing paragraphs 2.3.2 *and* 2.3.3 *have been renumbered* 2.2.2 *and* 2.2.3.

Part 6, Chapter 2
Construction Procedures

Effective date 1 July 2013

■ *Section 4*
Joints and connections

4.5 Fillet welds

(*Part only shown*)

4.5.1 The throat thickness of fillet welds is to be determined from:

~~*s* = the length of correctly proportioned weld fillet, clear of end craters, in mm, and is to be 10 x plate thickness, t_p, or 75 mm, whichever is the lesser, but in no case to be taken less than 40 mm~~

s = the length of correctly proportioned weld fillets, clear of end craters, in mm, and the fillet length is to be 10 × plate thickness or 40 mm, whichever is the greater, but need not exceed 75 mm.

Part 7, Chapter 2
Construction Procedures

Effective date 1 July 2013

■ *Section 4*
Joints and connections

4.5 Fillet welds

(*Part only shown*)

4.5.1 The throat thickness of fillet welds is to be determined from:

~~*s* = the length of correctly proportioned weld fillet, clear of end craters, in mm, and is to be 10 x plate thickness, t_p, or 75 mm, whichever is the lesser, but in no case to be taken less than 40 mm~~

s = the length of correctly proportioned weld fillets, clear of end craters, in mm, and the fillet length is to be 10 × plate thickness or 40 mm, whichever is the greater, but need not exceed 75 mm.

Part 8, Chapter 3
Scantling Determination for Mono-Hull Craft

Effective date 1 July 2013

■ *Section 1*
General

1.9 Plate and sandwich laminates

(*Part only shown*)

1.9.1 Unless otherwise specified in this Part, the bending moments, M_b and M_c, to be applied to a 1 cm length of panel, for both plate and sandwich laminates, subjected to lateral pressure are to be determined from:

~~p = design pressure head as required by Part 5, for the element of plate laminate under consideration, in kN/m^2.~~

ρ = for bottom and side shell of craft operating in non-displacement mode the greater of:
(a) $H_f\, S_f\, P_s$;
(b) $K_i\, H_f\, S_f\, C_f\, P_{dl}$;
(c) $H_f\, S_f\, G_f\, C_f\, P_f$;
in kN/m^2, where H_f, S_f, G_f, C_f, P_s, P_{dl}, P_f are as defined in Pt 5, Ch 3,2, and K_i as defined in 1.12.

For all other locations the design pressure is to be taken as required by Part 5 for the element of plate laminate under consideration, in kN/m^2.

1.12 Slamming Pressure Correction

1.12.1 The Rule bending moments, M_b and M_c, as determined by 1.9.1, may be reduced for panels subject to impact pressure, P_{dl}, in crafts operating in the non-displacement mode. For such panels, the following factor, K_i, may be applied:

$$K_i = 0{,}18 + \frac{1{,}8}{16\left(\frac{A_{pn}}{A_{rf}}\right) + 1{,}1}$$

but is not to be taken greater than 1 or less than 0,7

A_{pn} = area of plate laminate, in m^2, but is not to be taken as greater than $2\left(\frac{s}{1000}\right)^2$

A_{rf} = reference impact pressure area, in m^2,

$= 0{,}7\,\frac{\Delta}{T}$

Δ = displacement, in tonnes, as defined in Pt 5, Ch 2,2.2.2

T = draught, in metres, as defined in Pt 3, Ch 1,6.2.9

s is as defined in 1.5.1

Existing sub-Sections 1.12 *to* 1.31 *have been renumbered* 1.13 *to* 1.32.

~~1.13~~ 1.14 Mechanical properties sandwich laminates

~~1.13.11~~ 1.14.11 Where the Poisson's ratio, ν_f, for a particular facing laminate is known, the deflection, δ, of a flat sandwich panel with all edges assumed to be fully fixed~~,~~ and subjected to a uniform lateral pressure is to be determined from:

~~$$\delta = \frac{p\,b^2}{8t_c}\left(\frac{b^2\,(1-\nu_f^2)}{24E_{ms}\,t_s\,t_c} + \frac{1}{G}\right) \times 10^{-3} \text{ mm}$$~~

~~where the mean skin modulus, E_{ms}, is given by:~~

~~$$E_{ms} = \frac{\Sigma\,(E_p\,t_s)}{\Sigma\,t_s} \text{ N/mm}^2$$~~

~~E_p is E_{tp} or E_{op} whichever is the lesser.~~

~~where~~

~~ν_f, p, b, t_c, t_s, E_{tp}, E_{op} and G are as defined in 1.5.1 and E_{ms} is the mean modulus of the total skin thicknesses.~~

$$\delta = \frac{pb^2}{8}\left(\frac{b^2\,(1-\nu_f^2)}{48D_s}k_{db} + \frac{1}{Gt_c}\,k_{ds}\right) \times 10^{-3} \text{ mm}$$

where

k_{db} = bending deflection aspect ratio factor

$= 1{,}5 - \frac{1}{A_R}$ with A_R not to be taken greater than 2

k_{ds} = shear deflection aspect ratio factor

$= 1{,}2 - \frac{0{,}6}{A_R}$ with A_R not to be taken greater than 3

A_R = panel length/panel breadth

D_s = flexural rigidity of the sandwich panel per unit mm width

$$= \frac{E_{pi}\,t_{inner}\,E_{po}\,t_{outer}}{E_{pi}\,t_{inner} + E_{po}\,t_{outer}}\,(t_c + t_s)^2 \text{ Nmm}$$

E_{pi} is the lesser of E_{tps} or E_{cps} of the inner skin

E_{po} is the lesser of E_{tps} or E_{cps} of the outer skin

ν_f, p, b, t_c, t_s, E_{tps}, E_{cps} and G are as defined in 1.5.1

t_{inner} and t_{outer} are as defined in 1.7.1.

~~1.13.12~~ 1.14.12 Where the Poisson's ~~Ratio~~ ratio, ν_f, for a particular facing laminate is not known, the deflection, δ, of a flat sandwich panel with all edges assumed to be fully fixed, and subjected to a uniform lateral pressure is to be estimated from:

~~$$\delta = \frac{p\,b^2}{8t_c}\left(\frac{b^2}{24E_{ms}\,t_s\,t_c} + \frac{1}{G}\right) \times 10^{-3} \text{ mm}$$~~

~~where~~

~~δ, p, b, t_c, t_s, and G, are as defined in 1.5.1~~

~~E_{ms} is as defined in 1.13.11.~~

$$\delta = \frac{pb^2}{8}\left(\frac{b^2}{48D_s}k_{db} + \frac{1}{Gt_c}\,k_{ds}\right) \times 10^{-3} \text{ mm}$$

where

δ, p, b, t_c, and G are as defined in 1.5.1

D_s, k_{db}, k_{ds} are as defined in 1.14.11.

Part 8, Chapter 7
Failure Modes Control

Effective date 1 July 2013

■ *Section 2*
Deflection control

2.1 General

2.1.2 Notwithstanding the values in Table 7.2.1, the span/deflection ratio for panels subject to long-term static loading is to be less than 100.

Table 7.2.1 Limiting span/deflection ratio
(*Part only shown*)

Item	f_δ
Main/strength deck structures:	
• sandwich construction	~~150~~ 100
• secondary stiffening	200
• primary girders and web frames	250
• hatch covers	~~250~~ 100
Superstructure/deckhouse laminates:	
(a) Generally: • sandwich construction	~~100~~ 50
(b) Coachroof: • sandwich construction	~~150~~ 100
(c) House top: • sandwich construction	~~100~~ 50
(d) Lower/inner decks and house top subject to personnel loading:	
• sandwich construction	~~150~~ 100
Deep tank structures:	
(a) Laminates: • sandwich construction	~~150~~ 100
(b) Stiffeners: • secondary members	~~175~~ 100
• primary members	200
Watertight bulkhead structures:	
(a) Laminates: • sandwich construction	~~100~~ 50
(b) Stiffeners: • secondary members	~~125~~ 50
• primary members	150
Vehicle deck structures:	
(a) Laminates: • sandwich construction	~~150~~ 100
(b) Stiffeners: • secondary members	200
• primary members	250
Helicopter/flight decks:	
(a) Laminates: • sandwich construction	~~150~~ 100
(b) Stiffeners: • secondary members	200
• primary members	250

Cross-references

Section numbering in brackets reflects any Section renumbering necessitated by any of the Notices that update the current version of the Rules for Special Service Craft.

Part 8, Chapter 2

2.17.4	Ch 3, 1.20 *now reads* Ch 3, 1.21
2.18.4	Ch 3, 1.19 *now reads* Ch 3, 1.20
2.3.4	Ch 3, 1.18 *now reads* Ch 3, 1.19
5.19.1	Ch 3, 1.16 *now reads* Ch 3, 1.17

Part 8, Chapter 3

1.5.1	1.13.4 *now reads* 1.14.4
	1.13.5 *now reads* 1.14.5
	1.13.9 *now reads* 1.14.9
1.7.1	1.15 *now reads* 1.16
1.7.2	1.15 *now reads* 1.16
1.13.1 ***(1.14.1)***	1.13.2 *now reads* 1.14.2
1.13.10 ***(1.14.10)***	1.13.9 *now reads* 1.14.9
1.14.4 ***(1.15.4)***	1.14.3 *now reads* 1.15.3
1.15.1 ***(1.16.1)***	1.20.3 *now reads* 1.21.3
1.16.2 ***(1.17.2)***	1.14.3 *now reads* 1.15.3
	1.14.4 *now reads* 1.15.4
1.16.3 ***(1.17.3)***	1.16.2 *now reads* 1.17.2
1.20.3 ***(1.21.3)***	1.15 *now reads* 1.16
1.20.3 ***(1.21.3)***	1.18 *now reads* 1.19
1.23.1 ***(1.24.1)***	1.15.1 *now reads* 1.16.1
1.24.1 ***(1.25.1)***	1.17.51 *now reads* 1.18.5
1.24.4 ***(1.25.4)***	1.14 *now reads* 1.15
1.25.6 ***(1.26.6)***	1.16 *now reads* 1.17
1.25.7 ***(1.26.7)***	1.16 *now reads* 1.17
1.25.8 ***(1.26.8)***	1.16 *now reads* 1.17
3.2.1	1.12.6 *now reads* 1.13.6
3.3.1	1.12.6 *now reads* 1.13.6
3.4.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
3.4.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
3.5.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
3.5.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
4.2.1	1.14 *now reads* 1.15
4.4.4	1.14 *now reads* 1.15
4.5.4	1.14 *now reads* 1.15
4.6.2	1.14 *now reads* 1.15
4.7.2	1.14 *now reads* 1.15
4.8.3	1.14 *now reads* 1.15
4.9.4	1.14 *now reads* 1.15
4.10.4	1.14 *now reads* 1.15
4.11.2	1.14 *now reads* 1.15
4.12.2	1.14 *now reads* 1.15
4.13.3	1.14 *now reads* 1.15
4.19.5	1.14 *now reads* 1.15
5.2.4	1.16 *now reads* 1.17
5.3.5	1.16 *now reads* 1.17
5.4.4	1.16 *now reads* 1.17
5.6.5	1.18 *now reads* 1.19
5.7.4	1.29 *now reads* 1.30
6.3.1	1.16 *now reads* 1.17
6.4.4	1.16 *now reads* 1.17
6.6.2	1.16 *now reads* 1.17
6.9.3	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
6.9.5	1.13.2 *now reads* 1.14.2
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
	1.13.9 *now reads* 1.14.9
6.10.4	1.14 *now reads* 1.15
6.11.3	1.14 *now reads* 1.15
7.1.3	1.18 *now reads* 1.19
7.3.3	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
7.3.5	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
7.3.8	1.14 *now reads* 1.15
7.3.10	1.15 *now reads* 1.16
7.4.3	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
7.4.5	1.13.2 *now reads* 1.14.2
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
	1.13.9 *now reads* 1.14.9
7.4.8	1.14 *now reads* 1.15
7.4.10	1.15 *now reads* 1.16
8.3.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
8.3.4	1.13.2 *now reads* 1.14.2
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
	1.13.9 *now reads* 1.14.9
8.4.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
8.4.4	1.13.2 *now reads* 1.14.2
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
	1.13.9 *now reads* 1.14.9
8.6.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
8.6.4	1.13.2 *now reads* 1.14.2
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
	1.13.9 *now reads* 1.14.9
8.8.1	1.14 *now reads* 1.15
8.8.2	1.14 *now reads* 1.15
8.8.4	1.15 *now reads* 1.16
8.9.1	1.14 *now reads* 1.15
8.9.3	1.15 *now reads* 1.16
8.11.1	1.14 *now reads* 1.15
8.11.3	1.15 *now reads* 1.16
9.3.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4

9.3.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
9.4.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
9.4.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
9.5.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
9.5.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
9.6.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
9.6.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
9.7.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
9.7.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
9.8.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
9.8.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
9.10.1	1.14 *now reads* 1.15
9.10.2	1.14 *now reads* 1.15
9.10.4	1.15 *now reads* 1.16
9.11.1	1.14 *now reads* 1.15
9.11.2	1.14 *now reads* 1.15
9.11.4	1.15 *now reads* 1.16
9.12.1	1.14 *now reads* 1.15
9.12.2	1.14 *now reads* 1.15
9.12.4	1.15 *now reads* 1.16
9.13.2	1.14 *now reads* 1.15
9.13.3	1.14 *now reads* 1.15
9.13.5	1.15 *now reads* 1.16
9.14.1	1.14 *now reads* 1.15
9.14.2	1.14 *now reads* 1.15
9.14.4	1.15 *now reads* 1.16
9.15.1	1.14 *now reads* 1.15
9.15.2	1.14 *now reads* 1.15
9.15.6	1.15 *now reads* 1.16
9.16.1	1.14 *now reads* 1.15
9.16.2	1.14 *now reads* 1.15
9.16.4	1.15 *now reads* 1.16
9.20.3	1.15 *now reads* 1.16
9.25.3	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
9.25.5	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
9.25.7	1.14 *now reads* 1.15
9.25.9	1.15 *now reads* 1.16

Part 8, Chapter 4

3.3.3	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
3.5.4	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
3.5.6	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
3.7.3	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
3.7.5	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
4.2.4	1.14 *now reads* 1.15
4.3.4	1.14 *now reads* 1.15
4.4.2	1.14 *now reads* 1.15
4.5.2	1.14 *now reads* 1.15
4.6.3	1.14 *now reads* 1.15
4.12.4	1.14 *now reads* 1.15
4.13.4	1.14 *now reads* 1.15
4.14.2	1.14 *now reads* 1.15
4.15.2	1.14 *now reads* 1.15
4.16.3	1.14 *now reads* 1.15
4.22.4	1.14 *now reads* 1.15
4.23.4	1.14 *now reads* 1.15
4.24.2	1.14 *now reads* 1.15
4.25.2	1.14 *now reads* 1.15
4.26.3	1.14 *now reads* 1.15
5.3.4	1.16 *now reads* 1.17
5.4.4	1.16 *now reads* 1.17
5.5.4	1.16 *now reads* 1.17
6.3.1	1.16 *now reads* 1.17
6.4.4	1.16 *now reads* 1.17
6.5.2	1.16 *now reads* 1.17
8.4.2	1.12.1 *now reads* 1.13.1
	1.12.3 *now reads* 1.13.3
	1.12.4 *now reads* 1.13.4
8.4.4	1.13.2 *now reads* 1.14.2
	1.13.9 *now reads* 1.14.9
	1.13.7 *now reads* 1.14.7
	1.13.8 *now reads* 1.14.8
8.5.1	1.14 *now reads* 1.15
8.5.2	1.14 *now reads* 1.15
8.5.4	1.15 *now reads* 1.16

Cross-references

Part 8, Chapter 5

6.3.2 1.18 *now reads* 1.19

Part 8, Chapter 7

3.5.1 1.13.9 *now reads* 1.14.9

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